

Hydraulic analysis for box culvert systems

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INTRODUCTION

A typical storm drain system may consist of pipe systems in the upstream drainage reaches and box culvert systems in the downstream drainage reaches. An interactive computer program in designing storm drain pipe systems has been developed by Yen and Hromadka⁵. Implementation of the hydraulic analysis procedures to a box culvert system follows the same analog as the pipe systems. In the subject computer program, the hydraulic analysis first proceeds upstream. Therefore, the water depth is assumed to be greater than the critical depth in each drainage reach. A second analysis is then made by calculations in the downstream direction, where the depths are less than or equal to the critical depth in each drainage reach. Finally, the pressure plus momentum values for each of the two analyses are compared to determine the energy grade line (EGL) and hydraulic grade line (HGL) for the entire storm drain system. Pressure flow, nonpressure flow, hydraulic jumps, and minor losses in each drainage reach can be determined individually.

IMPLEMENTATIONS

The minor loss models, such as friction losses, manhole losses, sudden reduction/enlargement losses, transition losses and junction losses, can be easily implemented to the box system because all the minor loss models are functions of velocity heads.

A gradually varied flow model (Hromadka *et al.*⁴) for rectangular channel sections has been modified to analyze both pressure and non-pressure flow conditions for the box system. Water surface profile determination logic remains the same as the pipe system model (Yen and Hromadka⁵).

Finally, the output formats have been changed to accommodate the box culvert systems (see Appendix).

APPLICATION

An example problem was taken from Los Angeles Flood Control District (LAFCD) (Design Manual: Hydraulic) to illustrate the capability of the box systems model. Figure 1 depicts the plan and profile for the example problem. Table 1 compares the model estimated HGL and EGL to the LAFCD Manual's results. The pressure plus momentum balancing point was estimated at station 2+18 and station 2+10 by the model and LAFCD

Table 1. HGL and EGL for example problem

Section No.	Hydraulic Grade Line		Energy Grade Line	
	LAFCD Manual	Model estimated	LAFCD Manual	Model estimated
1	66.55	66.55	68.28	68.28
2	64.30	64.29	69.80	69.74
3	69.13	69.12	71.78	71.77
4	Junction	{ 69.82	71.99	71.98
	Structure	{ 70.22	72.07	72.10
5		72.04	73.75	73.74
6		71.99	73.81	73.81
7		72.81	74.38	74.23
8		73.47	75.04	74.74
9		73.72	75.29	75.04

Manual, respectively. At junction structure (section 4), the computer model defaulted junction losses to the manhole losses. Thus, a higher EGL was estimated by the model, i.e. 72.10 feet by the model and 72.07 feet by the LAFCD Manual. The model estimated gradually varied flow profiles were lower than the LAFCD Manual's estimated profiles. This is mainly because 25 energy balance locations (see Appendix) have been used in the model which resulted in more accurate water surface profiles.

DISCUSSIONS

The box culvert model can analyze the hydraulic jumps, pressure and non-pressure flow conditions in any drainage reach. This program provides the hydraulic engineer a better tool of designing box storm drain systems when pressure and non-pressure flow co-exist in the system. Further analyses on the junction and transition structures are needed in order to integrate the pipe and box culvert models into a general storm drain analysis model.

REFERENCES

- 1 Design Manual: Channel Hydraulics and Structures. Orange County Flood District, OCEMA, California, 1972
- 2 Design Manual: Hydraulic, Los Angeles County Flood Control District, Los Angeles, California, 1970
- 3 Design Manual, Los Angeles County Road Department, Los Angeles, California, 1972
- 4 Hromadka II, T. V., Becch, B. L. and Clements, J. M. Computational Hydraulics for Civil Engineers. Lighthouse Publication, Mission Viejo, California, 1988
- 5 Yen, C. C. and Hromadka II, T. V. Interactive hydraulic analysis for storm drain pipe systems. *Hydrosoft*, 1988, 1(4)

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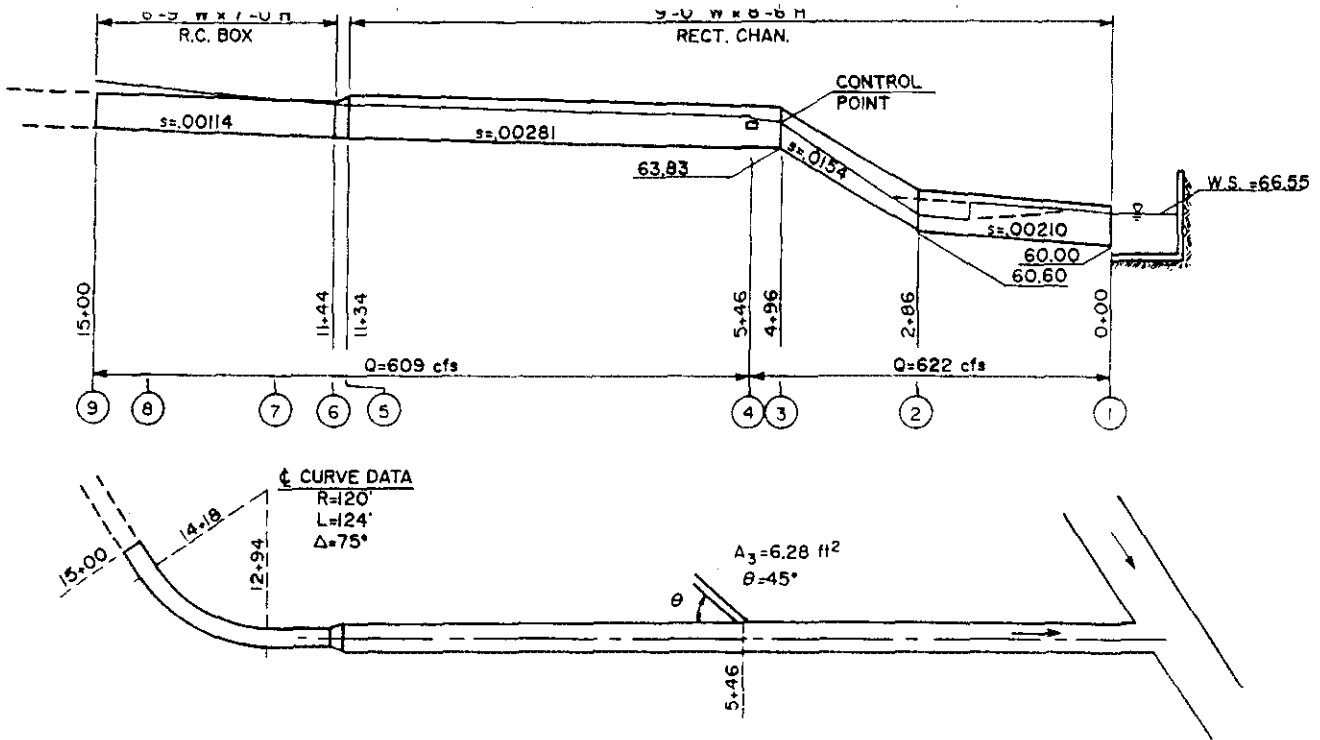


Fig. 1. Plan and profile for example problem

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GRADUALLY VARIED FLOW ANALYSIS FOR BOX SYSTEM
 NODAL POINT STATUS TABLE

(Note: "*" indicates nodal point data used.)

NODE NUMBER	MODEL PROCESS	UPSTREAM RUN		DOWNSTREAM RUN	
		PRESSURE HEAD(FT)	PRESSURE+ MOMENTUM(POUNDS)	FLOW DEPTH(FT)	PRESSURE+ MOMENTUM(POUNDS)
9.00-		7.46*	26888.19	5.32 Dc	23166.42
	} FRICTION				
8.00-		7.26*	26099.09	5.32 Dc	23166.42
	} FRICTION+BEND				
7.00-		6.78*	24659.67	5.32 Dc	23166.42
	} FRICTION				
6.00-		6.22*	23771.27	5.32 Dc	23166.42
	} TRANSITION				
5.00-		6.38*	23945.73	4.70	23193.86
	} FRICTION				
4.00-		6.27*	23780.55	5.22 Dc	22949.90
	} JUNCTION				
4.00-		5.57*	23666.96	5.29 Dc	23605.41
	} FRICTION				
3.00-		5.29 Dc	23605.41	5.29*Dc	23605.41
	} FRICTION				
2.00-		6.80	25233.02	3.69*	26399.63
	} FRICTION				
					} HYDRAULIC JUMP
1.00-		6.55*	24765.23	5.29 Dc	23605.41

MAXIMUM NUMBER OF ENERGY BALANCES USED IN EACH PROFILE = 25

NOTE: STEADY FLOW HYDRAULIC HEADFLOW CALCULATIONS BASED ON THE MOST CONSERVATIVE FORMULAE FROM THE CURRENT LACRD, LACFCD, AND OCEMA DESIGN MANUALS.

NODE 9.00 : HGL = < 73.505>;EGL= < 75.040>;FLOWLINE= < 66.040>

FLOW PROCESS FROM NODE 9.00 TO NODE 8.00 IS CODE = 1
UPSTREAM NODE 9.00 ELEVATION = 66.04 (FLOW IS UNDER PRESSURE)

CALCULATE FRICTION LOSSES(LACFCD):

BOX FLOW = 609.00 CFS
BOX BASEWIDTH = 8.75 FEET BOX HEIGHT = 7.00 FEET
BOX LENGTH = 82.00 FEET MANNING'S N = .01400
SF=(Q/K)**2 = ((609.00)/(10128.360))**2 = .00362
HF=L*SF = (82.00)*(.00362) = .296

NODE 8.00 : HGL = < 73.208>;EGL= < 74.744>;FLOWLINE= < 65.950>

FLOW PROCESS FROM NODE 8.00 TO NODE 7.00 IS CODE = 3
UPSTREAM NODE 8.00 ELEVATION = 65.95 (FLOW UNSEALS IN REACH)

CALCULATE BOX-BEND LOSSES(OCEMA):

BOX FLOW = 609.00 CFS
BOX BASEWIDTH = 8.75 FEET BOX HEIGHT = 7.00 FEET
CENTRAL ANGLE = 75.000 DEGREES MANNING'S N = .01400
BOX LENGTH = 124.00 FEET BEND COEFFICIENT(KB) = .11625
ADJUSTED CENTRAL ANGLE = (75.000)*(32.17/ 124.00) = 19.460
FLOW VELOCITY = 9.94 FEET/SEC. VELOCITY HEAD = 1.535 FEET
HB=KB*(VELOCITY HEAD) = (.116)*(1.535) = .178
SF= .00274
HF=L*SF = (124.00)*(.00274) = .340
TOTAL HEAD LOSSES = HB + HF = (.178)+(.340) = .518
==> NORMAL FLOW IS PRESSURE FLOW

CRITICAL DEPTH(FT) = 5.32

DOWNSTREAM CONTROL ASSUMED FLOWDEPTH(FT) = 6.78

GRADUALLY VARIED FLOW PROFILE COMPUTED INFORMATION:

DISTANCE FROM CONTROL(FT)	FLOW DEPTH (FT)	VELOCITY (FT/SEC)	SPECIFIC ENERGY(FT)	PRESSURE+ MOMENTUM(POUNDS)
.000	6.778	10.266	8.415	24659.67
3.272	6.786	10.253	8.420	24676.73
6.576	6.795	10.239	8.424	24693.88
9.911	6.804	10.226	8.429	24711.11
13.278	6.813	10.212	8.434	24728.43
16.678	6.822	10.199	8.438	24745.82
20.111	6.831	10.186	8.443	24763.31
23.576	6.840	10.173	8.448	24780.88
27.074	6.849	10.159	8.452	24798.53
30.605	6.858	10.146	8.457	24816.27
34.170	6.867	10.133	8.462	24834.08
37.768	6.875	10.120	8.467	24851.99
41.401	6.884	10.107	8.471	24869.97
45.067	6.893	10.094	8.476	24888.04
48.768	6.902	10.081	8.481	24906.20
52.504	6.911	10.068	8.486	24924.43

56.275	6.920	10.055	8.491	24942.75
60.081	6.929	10.042	8.496	24961.15
63.922	6.938	10.029	8.500	24979.63
67.799	6.947	10.016	8.505	24998.20
71.712	6.956	10.003	8.510	25016.84
75.661	6.964	9.991	8.515	25035.57
79.647	6.973	9.978	8.520	25054.38
83.670	6.982	9.965	8.525	25073.27
87.730	6.991	9.952	8.530	25092.25
91.827	7.000	9.940	8.535	25111.30
==> FLOW IS UNDER PRESSURE				
124.000	7.258	9.943	8.794	39476.09

NODE 7.00 : HGL = (72.588);EGL= (74.225);FLOWLINE= (65.810)

FLOW PROCESS FROM NODE 7.00 TO NODE 6.00 IS CODE = 1
 UPSTREAM NODE 7.00 ELEVATION = 65.81 (FLOW IS SUBCRITICAL)

CALCULATE FRICTION LOSSES(LACFCD):

BOX FLOW = 609.00 CFS
 BOX BASEWIDTH = 8.75 FEET BOX HEIGHT = 7.00 FEET
 BOX LENGTH = 150.00 FEET MANNING'S N = .01400
 ==> NORMAL FLOW IS PRESSURE FLOW

CRITICAL DEPTH(FT) = 5.32

DOWNSTREAM CONTROL ASSUMED FLOWDEPTH(FT) = 6.22

GRADUALLY VARIED FLOW PROFILE COMPUTED INFORMATION:

DISTANCE FROM CONTROL(FT)	FLOW DEPTH (FT)	VELOCITY (FT/SEC)	SPECIFIC ENERGY(FT)	PRESSURE+ MOMENTUM(POUNDS)
.000	6.223	11.181	8.165	23771.27
5.904	6.254	11.126	8.177	23811.55
12.072	6.285	11.071	8.189	23853.00
18.510	6.316	11.016	8.202	23895.62
25.223	6.347	10.962	8.214	23939.39
32.217	6.378	10.909	8.227	23984.32
39.498	6.409	10.856	8.240	24030.38
47.073	6.440	10.803	8.254	24077.58
54.947	6.471	10.752	8.268	24125.90
63.128	6.503	10.700	8.282	24175.33
71.623	6.534	10.649	8.296	24225.86
80.438	6.565	10.599	8.310	24277.50
89.580	6.596	10.549	8.325	24330.22
99.059	6.627	10.499	8.340	24384.02
108.880	6.658	10.450	8.355	24438.90
119.053	6.689	10.402	8.370	24494.84
129.586	6.720	10.354	8.386	24551.84
140.487	6.751	10.306	8.402	24609.89
150.000	6.778	10.266	8.415	24659.67

NODE 6.00 : HGL = (71.863);EGL= (73.805);FLOWLINE= (65.640)

FLOW PROCESS FROM NODE 6.00 TO NODE 5.00 IS CODE = 9
 UPSTREAM NODE 6.00 ELEVATION = 65.64 (FLOW IS SUBCRITICAL)

CALCULATE TRANSITION LOSSES(LACFCD):

BOX FLOW = 609.00 CFS
 TRANSITION STRUCTURE LENGTH = 10.00 FEET
 TOTAL-ANGLE-OF-TRANSITION = 1.430 DEGREES

BOX	BASEWIDTH (FEET)	HEIGHT (FEET)	FRICTION FACTOR	VELOCITY (FT/SEC)	VELOCITY HEAD (FEET)
UPSTREAM	8.75	7.00	.01400	11.18	1.94
DOWNSTREAM	9.00	8.50	.01400	10.61	1.75

HT = .2*(V1*V1-V2*V2)/64.4
 TRANSITION LOSS COEFFICIENT = .20000 TRANSITION LOSS = .039
 AVERAGE TRANSITION STRUCTURE FRICTION SLOPE ASSUMED = .00298
 HF = L*SF = (10.00)*(.00298) = .030
 TOTAL LOSSES = (HT)+(HF) = (.039)+(.030) = .069

NODE 5.00 : HGL = < 71.989>;EGL= < 73.736>;FLOWLINE= < 65.610>

FLOW PROCESS FROM NODE 5.00 TO NODE 4.00 IS CODE = 1
 UPSTREAM NODE 5.00 ELEVATION = 65.61 (FLOW IS SUBCRITICAL)

CALCULATE FRICTION LOSSES(LACFCD):

BOX FLOW = 609.00 CFS
 BOX BASEWIDTH = 9.00 FEET BOX HEIGHT = 8.50 FEET
 BOX LENGTH = 588.00 FEET MANNING'S N = .01400

NORMAL DEPTH(FT) = 6.41 CRITICAL DEPTH(FT) = 5.22

DOWNSTREAM CONTROL ASSUMED FLOWDEPTH(FT) = 6.27

GRADUALLY VARIED FLOW PROFILE COMPUTED INFORMATION:

DISTANCE FROM CONTROL (FT)	FLOW DEPTH (FT)	VELOCITY (FT/SEC)	SPECIFIC ENERGY(FT)	PRESSURE+ MOMENTUM(POUNDS)
.000	6.273	10.783	8.080	23780.55
15.501	6.279	10.774	8.082	23788.82
31.746	6.284	10.764	8.085	23797.13
48.801	6.290	10.755	8.087	23805.48
66.741	6.295	10.745	8.089	23813.87
85.654	6.301	10.736	8.092	23822.29
105.638	6.306	10.726	8.094	23830.75
126.810	6.312	10.717	8.097	23839.24
149.305	6.317	10.708	8.099	23847.77
173.284	6.323	10.698	8.101	23856.34
198.939	6.329	10.689	8.104	23864.94
226.501	6.334	10.680	8.106	23873.58
256.252	6.340	10.670	8.109	23882.26
288.544	6.345	10.661	8.111	23890.97
323.820	6.351	10.652	8.114	23899.72
362.648	6.356	10.642	8.116	23908.51
405.778	6.362	10.633	8.118	23917.33
454.226	6.367	10.624	8.121	23926.19
509.416	6.373	10.615	8.123	23935.08
573.431	6.378	10.606	8.126	23944.01
588.000	6.379	10.604	8.126	23945.73

NODE 4.00 : HGL = < 70.293>;EGL= < 72.100>;FLOWLINE= < 64.020>

FLOW PROCESS FROM NODE 4.00 TO NODE 4.00 IS CODE = 5
 UPSTREAM NODE 4.00 ELEVATION = 64.02 (FLOW IS SUBCRITICAL)

CALCULATE JUNCTION LOSSES:

BOX	FLOW (CFS)	BASEWIDTH (FEET)	HEIGHT (FEET)	SLOPE (DECIMAL)	FRICTION FACTOR	ANGLE (DEGREES)	FLOWLINE ELEVATION
UPSTREAM	609.00	9.00	8.50	.00281	.0140	.00	64.02
DOWNSTREAM	622.00	9.00	8.50	.00281	.0140	-	64.02
LATERAL #1	13.00	3.14	2.00	.00281	.0140	45.00	66.00
LATERAL #2	.00	.00	.00	.00000	.0000	.00	.00
Q5	.00==Q5 EQUALS BASIN INPUT==						

NORMAL AND CRITICAL DEPTH INFORMATION:

BOX	CRITICAL DEPTH (FEET)	NORMAL DEPTH (FEET)
UPSTREAM	5.220	6.316
DOWNSTREAM	5.294	6.421
LATERAL #1	.810	1.016
LATERAL #2	.000	.000

LACFCD AND OCEMA FLOW JUNCTION FORMULAE USED:

$$DY = (Q2*V2 - Q1*V1*\cos(\Delta1) - Q3*V3*\cos(\Delta3) - Q4*V4*\cos(\Delta4)) / ((A1+A2)*16.1)$$

JUNCTION LENGTH = 1.00 FEET

FRICTION LOSSES = .000 FEET ENTRANCE LOSSES = .000 FEET

MANHOLE LOSSES = .05*(DOWNSTREAM VELOCITY HEAD) = .05*(2.39) = .120 FEET

JUNCTION LOSSES = (MANHOLE LOSSES)+(FRICTION LOSS)+(ENTRANCE LOSSES)

JUNCTION LOSSES = (.120)+(.000)+(.000) = .120

* USED MANHOLE LOSSES FOR THOMPSON MOMENTUM LOSSES AND MODIFIED FLOWDEPTH FOR ASSUMED JUNCTION LOSSES.

NODE 4.00 : HGL = < 69.588>; EGL = < 71.980>; FLOWLINE = < 64.020>

FLOW PROCESS FROM NODE 4.00 TO NODE 3.00 IS CODE = 1
 UPSTREAM NODE 4.00 ELEVATION = 64.02 (FLOW IS SUBCRITICAL)

CALCULATE FRICTION LOSSES(LACFCD):

BOX FLOW = 622.00 CFS
 BOX BASEWIDTH = 9.00 FEET BOX HEIGHT = 8.50 FEET
 BOX LENGTH = 50.00 FEET MANNING'S N = .01400

NORMAL DEPTH(FT) = 5.71 CRITICAL DEPTH(FT) = 5.29

DOWNSTREAM CONTROL ASSUMED FLOWDEPTH(FT) = 5.29

GRADUALLY VARIED FLOW PROFILE COMPUTED INFORMATION:

DISTANCE FROM CONTROL(FT)	FLOW DEPTH (FT)	VELOCITY (FT/SEC)	SPECIFIC ENERGY(FT)	PRESSURE+ MOMENTUM(POUNDS)
.000	5.294	13.052	7.940	23605.41
.098	5.310	13.011	7.940	23605.65
.401	5.327	12.970	7.941	23606.34
.929	5.343	12.930	7.941	23607.50
1.702	5.360	12.890	7.942	23609.11
2.744	5.377	12.850	7.942	23611.18
4.081	5.393	12.810	7.943	23613.70
5.747	5.410	12.771	7.944	23616.66
7.779	5.427	12.732	7.945	23620.08
10.220	5.443	12.693	7.946	23623.94
13.124	5.460	12.654	7.948	23628.23
16.553	5.476	12.616	7.949	23632.97
20.587	5.493	12.578	7.951	23638.14

20.021	3.510	12.540	7.953	23643.75
30.878	5.526	12.502	7.955	23649.79
37.413	5.543	12.464	7.957	23656.25
45.134	5.560	12.427	7.959	23663.14
50.000	5.568	12.407	7.960	23666.96

NODE 3.00 : HGL = < 69.124>;EGL= < 71.770>;FLOWLINE= < 63.830>

FLOW PROCESS FROM NODE 3.00 TO NODE 2.00 IS CODE = 1
 UPSTREAM NODE 3.00 ELEVATION = 63.83 (FLOW IS SUPERCRITICAL)

CALCULATE FRICTION LOSSES(LACFCD):

BOX FLOW = 622.00 CFS
 BOX BASEWIDTH = 9.00 FEET BOX HEIGHT = 8.50 FEET
 BOX LENGTH = 210.00 FEET MANNING'S N = .01400

NORMAL DEPTH(FT) = 3.38 CRITICAL DEPTH(FT) = 5.29

UPSTREAM CONTROL ASSUMED FLOWDEPTH(FT) = 5.29

GRADUALLY VARIED FLOW PROFILE COMPUTED INFORMATION:

DISTANCE FROM CONTROL (FT)	FLOW DEPTH (FT)	VELOCITY (FT/SEC)	SPECIFIC ENERGY (FT)	PRESSURE+ MOMENTUM (POUNDS)
.000	5.294	13.052	7.940	23605.41
.158	5.217	13.243	7.942	23610.37
.654	5.141	13.439	7.947	23625.45
1.520	5.064	13.642	7.956	23650.94
2.794	4.988	13.851	7.969	23687.19
4.523	4.912	14.066	7.986	23734.54
6.755	4.835	14.288	8.007	23793.36
9.552	4.759	14.517	8.034	23864.05
12.982	4.683	14.754	8.065	23947.02
17.130	4.606	14.999	8.102	24042.73
22.095	4.530	15.251	8.144	24151.65
27.996	4.454	15.513	8.193	24274.30
34.981	4.377	15.783	8.248	24411.21
43.234	4.301	16.064	8.310	24562.99
52.985	4.225	16.354	8.380	24730.24
64.532	4.148	16.655	8.458	24913.66
78.268	4.072	16.967	8.545	25113.96
94.726	3.996	17.291	8.641	25331.93
114.653	3.919	17.628	8.748	25568.39
139.144	3.843	17.979	8.865	25824.28
169.898	3.767	18.343	8.994	26100.55
209.763	3.690	18.722	9.137	26398.29
210.000	3.690	18.724	9.137	26399.63

NODE 2.00 : HGL = < 64.290>;EGL= < 69.737>;FLOWLINE= < 60.600>

FLOW PROCESS FROM NODE 2.00 TO NODE 1.00 IS CODE = 1
 UPSTREAM NODE 2.00 ELEVATION = 60.60 (HYDRAULIC JUMP OCCURS)

CALCULATE FRICTION LOSSES(LACFCD):

BOX FLOW = 622.00 CFS
 BOX BASEWIDTH = 9.00 FEET BOX HEIGHT = 8.50 FEET
 BOX LENGTH = 286.00 FEET MANNING'S N = .01400

HYDRAULIC JUMP: DOWNSTREAM RUN ANALYSIS RESULTS

NORMAL DEPTH(FT) = 7.21 CRITICAL DEPTH(FT) = 5.29

UPSTREAM CONTROL ASSUMED FLOWDEPTH(FT) = 3.69

GRADUALLY VARIED FLOW PROFILE COMPUTED INFORMATION:

DISTANCE FROM CONTROL(FT)	FLOW DEPTH (FT)	VELOCITY (FT/SEC)	SPECIFIC ENERGY(FT)	PRESSURE+ MOMENTUM(POUNDS)
.000	3.690	18.724	9.137	26399.63
12.344	3.754	18.404	9.017	26147.94
24.410	3.818	18.095	8.906	25911.51
36.186	3.882	17.796	8.803	25689.72
47.662	3.946	17.507	8.709	25481.96
58.824	4.011	17.227	8.622	25287.66
69.660	4.075	16.956	8.542	25106.31
80.156	4.139	16.693	8.468	24937.40
90.296	4.203	16.438	8.401	24780.48
100.066	4.267	16.191	8.340	24635.10
109.448	4.331	15.951	8.285	24500.86
118.425	4.395	15.718	8.234	24377.37
126.977	4.460	15.492	8.189	24264.26
135.085	4.524	15.273	8.148	24161.20
142.725	4.588	15.059	8.111	24067.85
149.876	4.652	14.851	8.079	23983.91
156.512	4.716	14.649	8.051	23909.10
162.604	4.780	14.453	8.026	23843.14
168.125	4.845	14.261	8.005	23785.76
173.042	4.909	14.075	7.987	23736.72
177.321	4.973	13.893	7.972	23695.80
180.924	5.037	13.717	7.960	23662.76
183.811	5.101	13.544	7.951	23637.39
185.936	5.165	13.376	7.945	23619.51
187.251	5.229	13.212	7.942	23608.91
187.703	5.294	13.052	7.940	23605.41
286.000	5.294	13.052	7.940	23605.41

HYDRAULIC JUMP: UPSTREAM RUN ANALYSIS RESULTS

DOWNSTREAM CONTROL ASSUMED FLOWDEPTH(FT) = 6.55

GRADUALLY VARIED FLOW PROFILE COMPUTED INFORMATION:

DISTANCE FROM CONTROL(FT)	FLOW DEPTH (FT)	VELOCITY (FT/SEC)	SPECIFIC ENERGY(FT)	PRESSURE+ MOMENTUM(POUNDS)
.000	6.550	10.548	8.279	24765.23
22.319	6.576	10.506	8.291	24811.27
46.071	6.603	10.464	8.304	24858.11
71.384	6.629	10.423	8.317	24905.73
98.404	6.655	10.381	8.330	24954.14
127.297	6.681	10.341	8.343	25003.32
158.255	6.708	10.300	8.356	25053.28
191.502	6.734	10.260	8.370	25104.01
227.300	6.760	10.220	8.383	25155.50
265.959	6.787	10.180	8.397	25207.76
286.000	6.799	10.162	8.403	25233.02

END OF HYDRAULIC JUMP ANALYSIS

* NOTE: PRESSURE + MOMENTUM BALANCE OCCURS 218.52 FEET FROM NODE 1.00

NODE 1.00 : HGL = \ 66.5507;EGL= (68.279);FLOWLINE= (60.000)

DOWNSTREAM BOX FLOW CONTROL DATA:

NODE NUMBER = 1.00 FLOWLINE ELEVATION = 60.00

BOX FLOW = 622.00 CFS

BOX BASEWIDTH = 9.00 FEET BOX HEIGHT = 8.50 FEET

ASSUMED DOWNSTREAM CONTROL HGL = 66.550

END OF GRADUALLY VARIED FLOW ANALYSIS